Atmospheric Optical Turbulence Characterization for the Airborne Laser Using Combined Measurement and Simulation Techniques

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ERDC MSRC



T3E and archival storage resources:

ERDC and **NAVO**

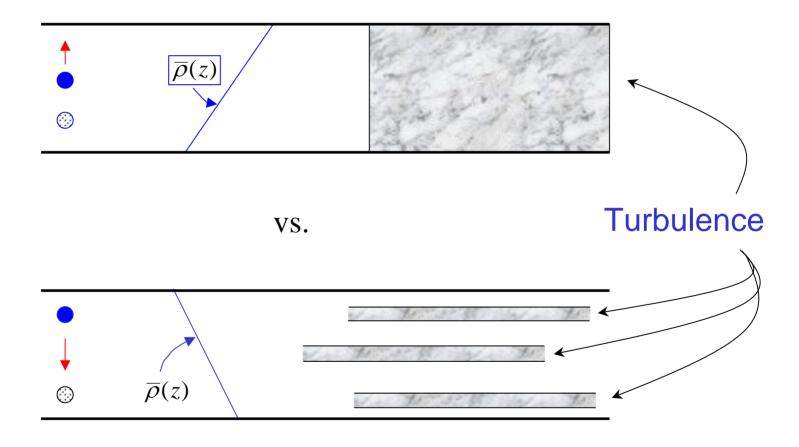


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Overview of our ABL-Component Objectives

- ☐ Use numerical simulations to improve/augment atmospheric turbulence characterization so that:
 - <u>phase-screen specification</u> for optical propagation simulations may be evaluated and possibly improved, and
 - more intelligent modeling may proceed, admitting simulation of larger-scale processes and the development of a reliable atmospheric decision aid.

The Problem with Stratified Fluids



■ Range of scales: from 200km to 100m (or smaller).

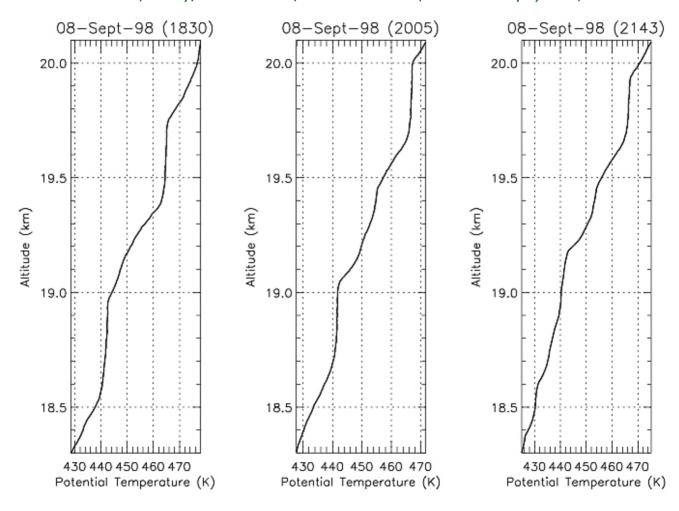
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- Non-Kolmogorov: current sub-grid-scale (SGS) turbulence parameterization schemes are inadequate for stable stratification.

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- Non-Kolmogorov: current sub-grid-scale (SGS) turbulence parameterization schemes are inadequate for stable stratification.
- □ Combined numerical/observational studies are feasible for developing improved phase-screen descriptions, but simulations of isolated turbulent layers still require state-of-the-art techniques.

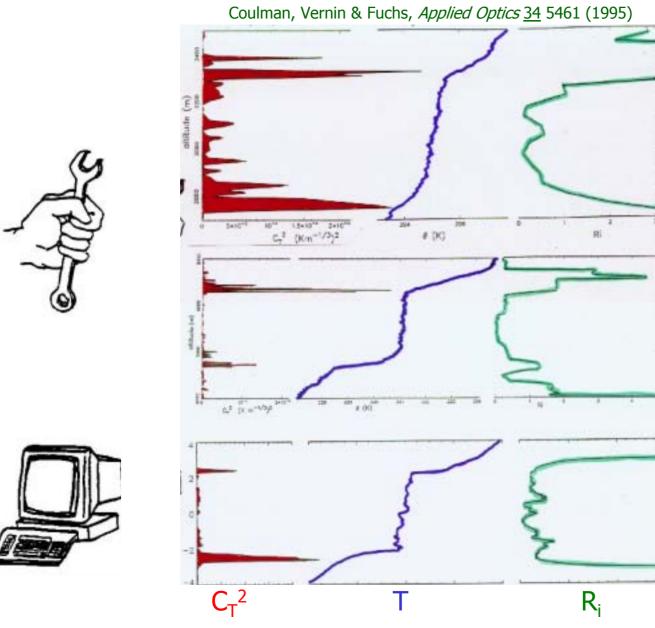
Potential-Temperature Steps in the Stratosphere



Chen, Kelley, Gibson-Wilde, Werne & Beland, Annales Geophysicae, 2001



Wind shear: Balloon Comparison

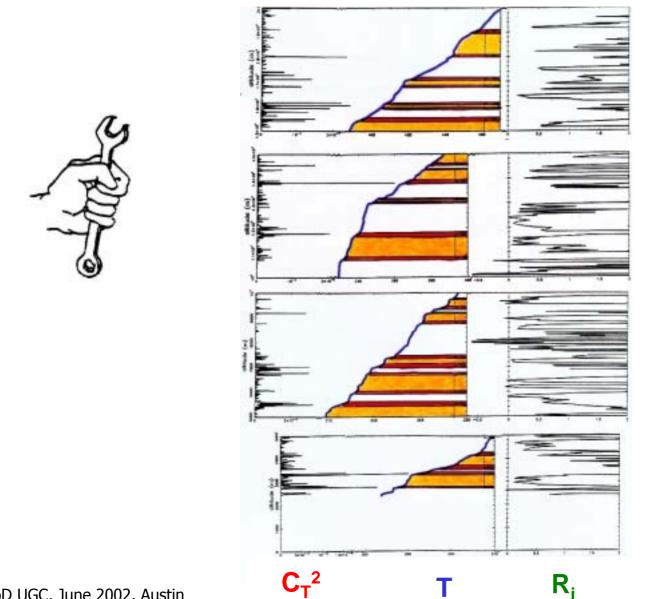


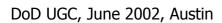
DoD UGC, June 2002, Austin

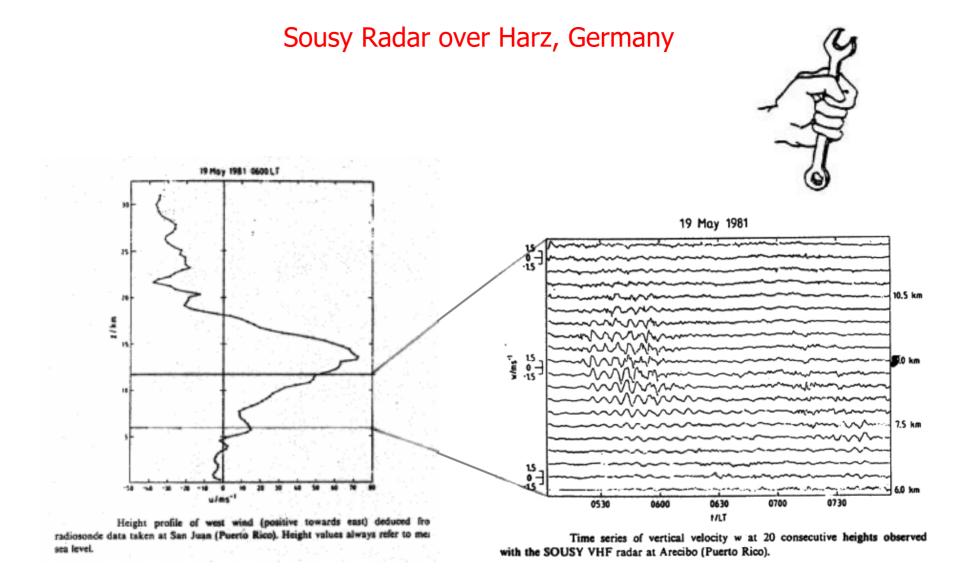
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Mixing Layers through the Troposphere and Stratosphere

Coulman, Vernin & Fuchs, Applied Optics 34 5461 (1995)



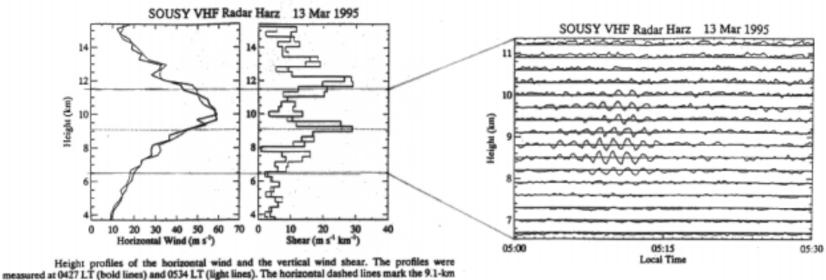




Chilson, Muschinski & Schmidt, Radio Science, 32, 1997

Sousy Radar at Arecibo

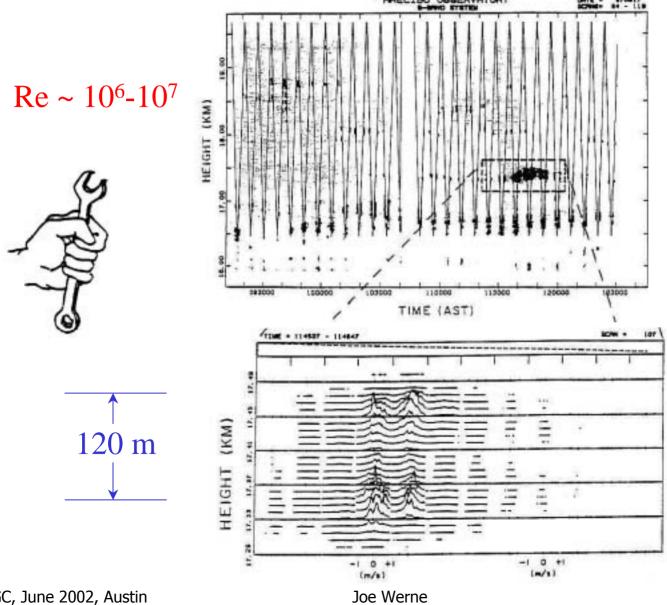


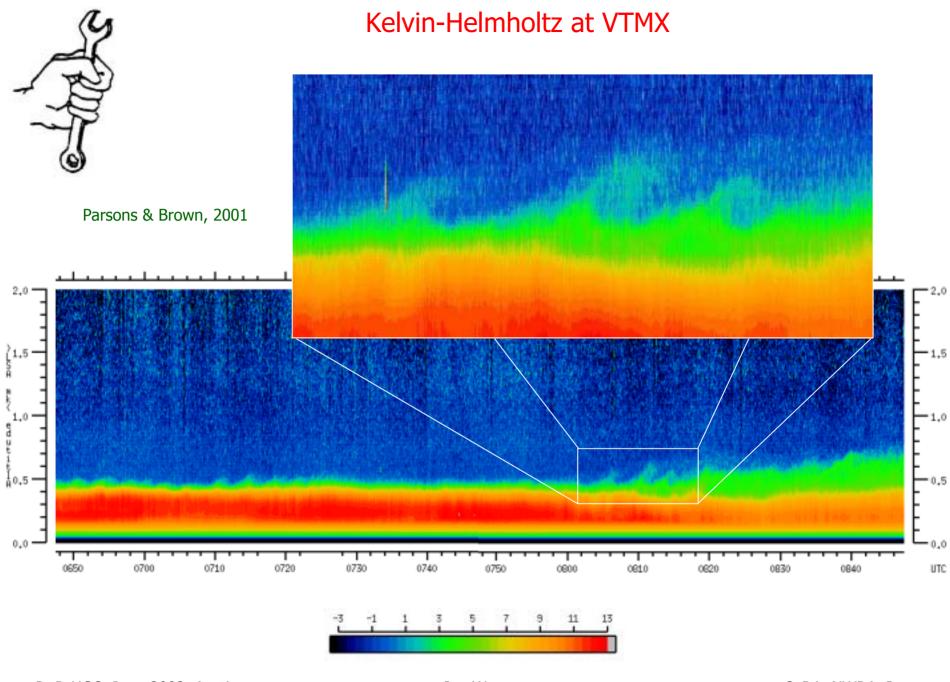


Unfiltered radial velocities measured while the radar beam was oriented vertically. The large-amplitude oscillations mark the occurrence of a Kelvin-Helmholtz instability (KHI). The velocities have been scaled such that 1 m s⁻¹ corresponds to 100 m.

Rüster and Klostermeyer, Geophys. Astrophys. Fluid Dynamics, 26, 1983

height.



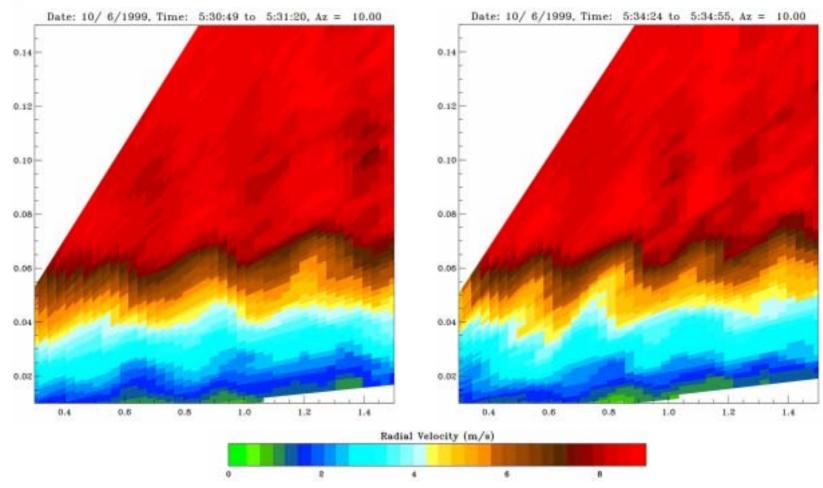


DoD UGC, June 2002, Austin Joe Werne CoRA, NWRA, Inc.





Blumen, Banta, Burns, Fritts, Newsom, Poulos, Sun, Dyn. Atmos. Oceans, 2001

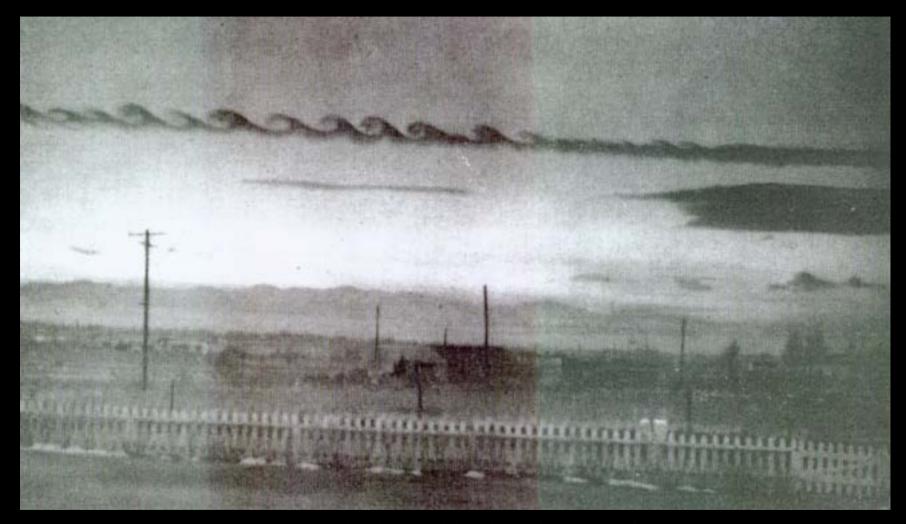




Estes Park, Colorado, 1979 (photo by Bob Perney)



Colorado Springs, Colorado, 2000 (photo by Tye Parzybok)



Denver, Colorado, 1953 (photo by Paul E. Branstine)



Noctilucent Clouds, Kustavi, Finland, 1989 (photo by Pekka Parviainen)

DNS Efforts

- Validate simulations
- ☐ Characterize/quantify atmospheric turbulence

Phase Screen Specification

- ☐ Combine observation and simulation for long paths
- Quantify non-Kolmogorov effects

Turbulence Simulation Algorithm Development

- SGS parameterizations
- Better upper boundary conditions

DNS Efforts

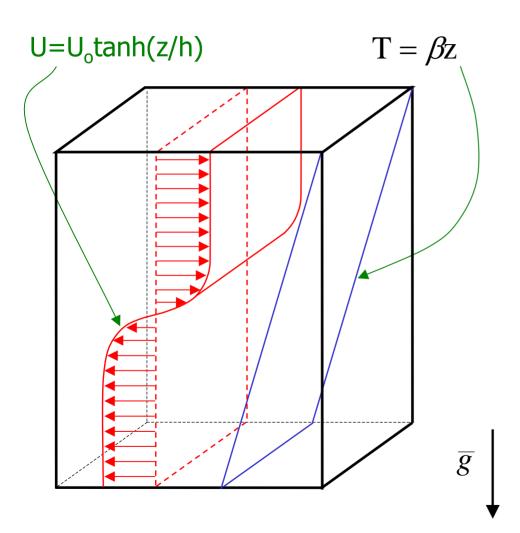
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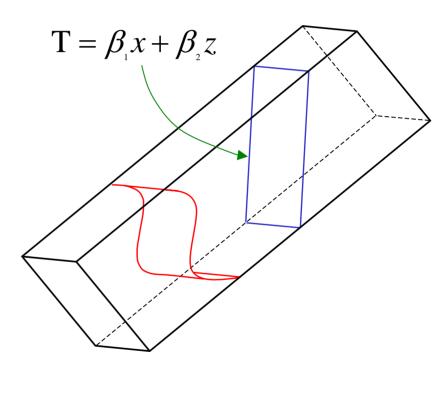
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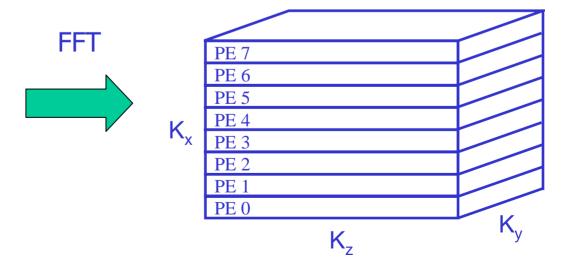


3D Incompressible Navier-Stokes Solver

$$\partial_t \mathbf{u} + \boldsymbol{\omega} \times \mathbf{u} = \mathbf{R} \mathbf{e}^{-1} \Delta \mathbf{u} - \nabla \mathbf{P} + \mathbf{R}_i \boldsymbol{\Theta}$$
$$\partial_t \boldsymbol{\Theta} + \mathbf{u} \cdot \nabla \boldsymbol{\Theta} = \mathbf{P} \mathbf{e}^{-1} \Delta \boldsymbol{\Theta}$$

 $\nabla \cdot \mathbf{u} = 0$

- Stream-function/vorticity formulation
- Fully spectral (3D FFT's = 75% computation)
- Radix 2,3,4,5 FFT's
- Spectral modes and NCPUs must be commensurate
- Communication: shmem, global transpose, data reduction
- Parallel I/O every $\sim 60 \, \delta t$



X

Headaches, woes, and what to do about them.

Headaches, woes, and what to do about them.

- Typical 20-hour run on 500 processors generates 800 Gigabytes of data and over 70,000 individual files.
- Interactive performance can be poor during large production runs.
- Center non-uniformity contributes to drudgery.

Headaches, woes, and what to do about them.

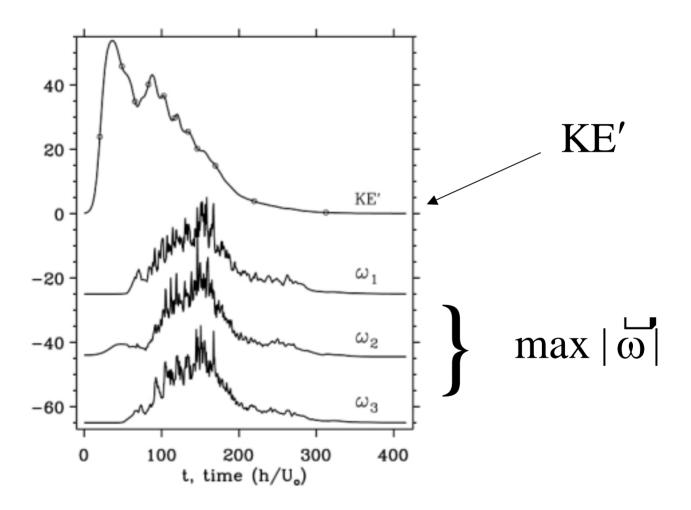
- Typical 20-hour run on 500 processors generates 800 Gigabytes of data and over 70,000 individual files.
- Interactive performance can be poor during large production runs.
- Center non-uniformity contributes to drudgery.
- Elaborate scripts automate job specification, source-code editing, compilation, and submission as well runtime data transfers and migration off-line to archival storage.
- FORTRAN code and accompanying Perl scripts run without modification at 6 supercomputer centers and 4 MPP architectures (T3E, O3k, SP, Compag).
- DoD has adopted our batch-preparation and archival-storage routines as a standard (PST, Werne, Gourlay).

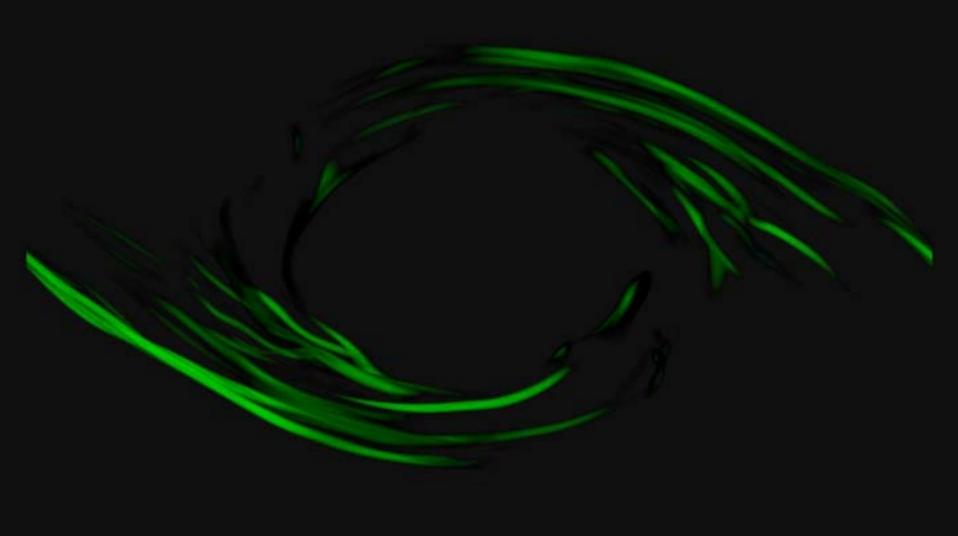
Vortex-Tube Morphology Werne, Meyer, Bizon & Fritts, 2001 Wind shear Gravity-wave breaking

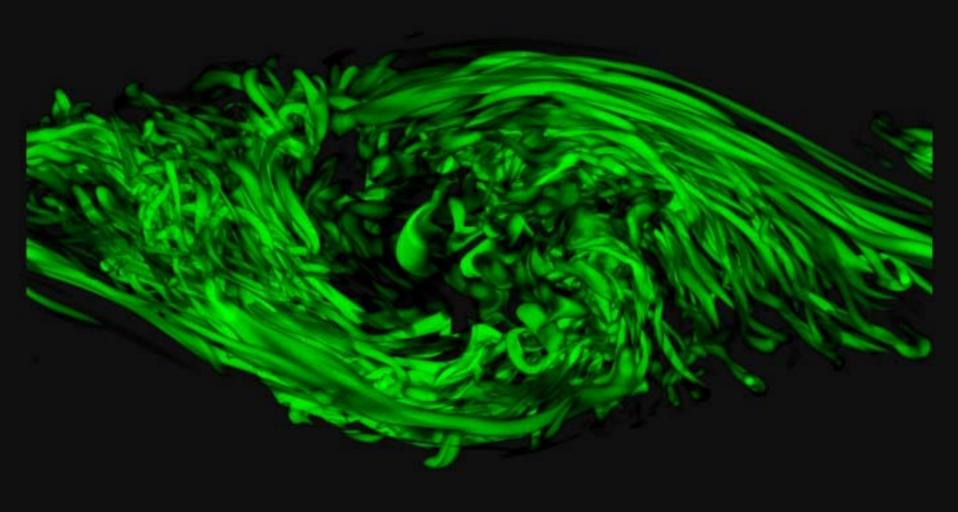
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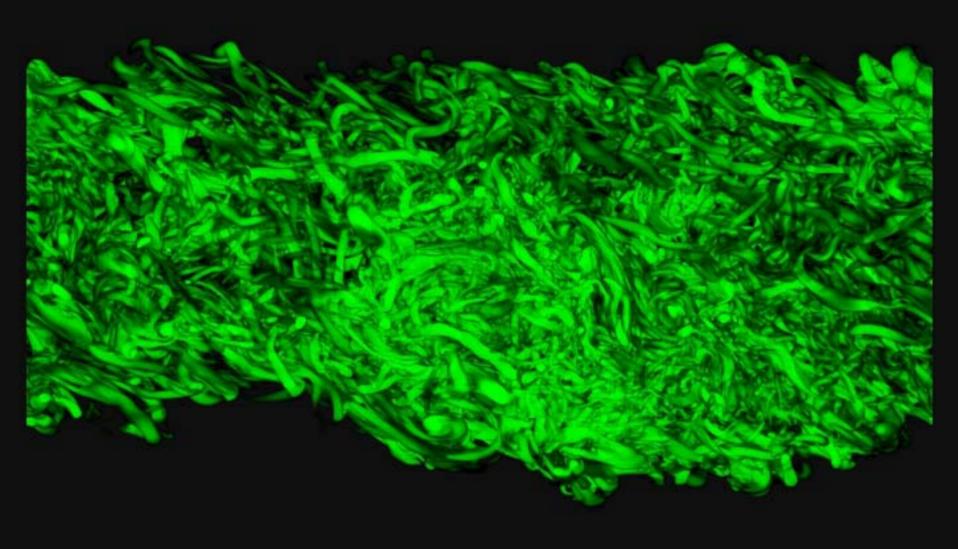


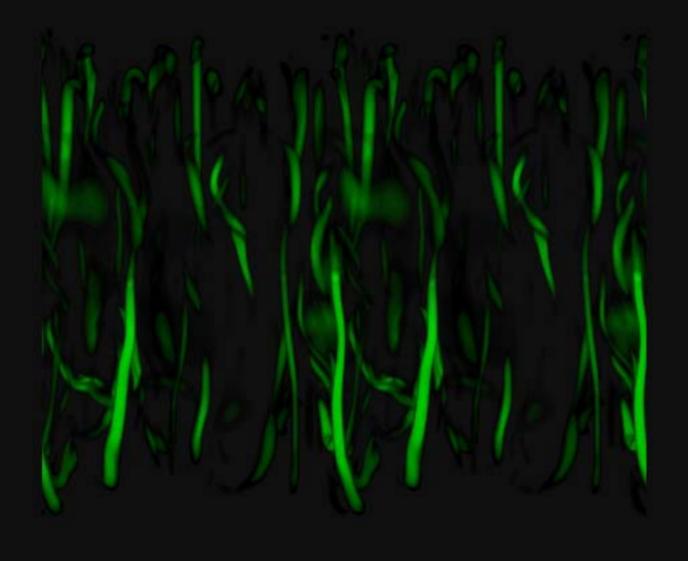
Kelvin-Helmholtz: Evolution

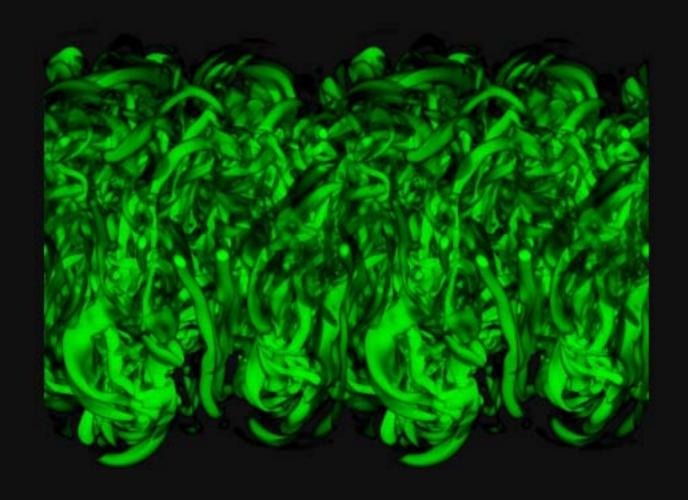


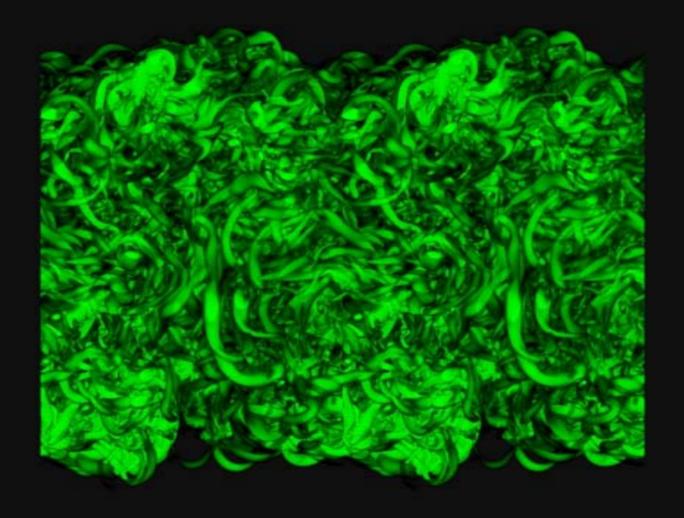


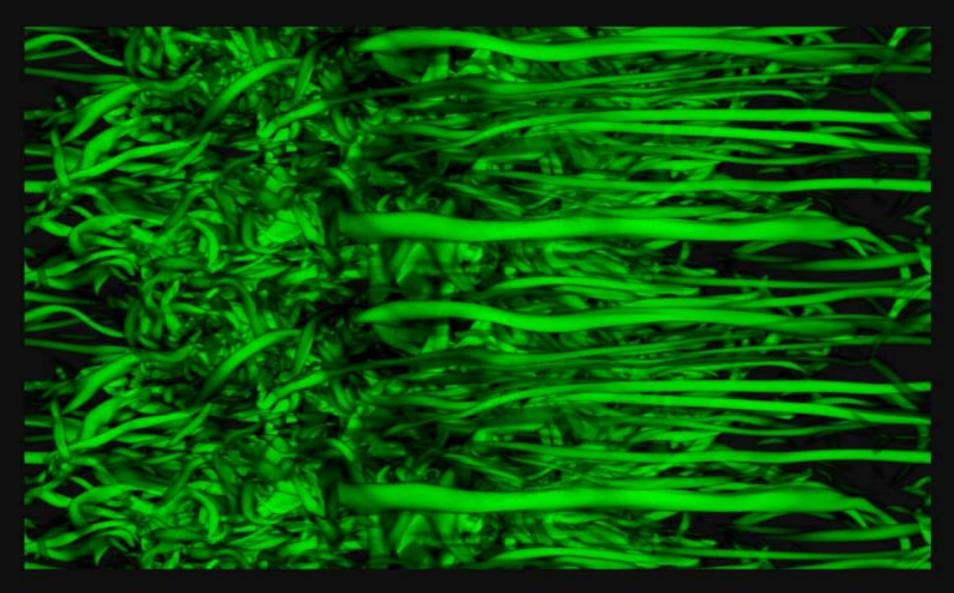


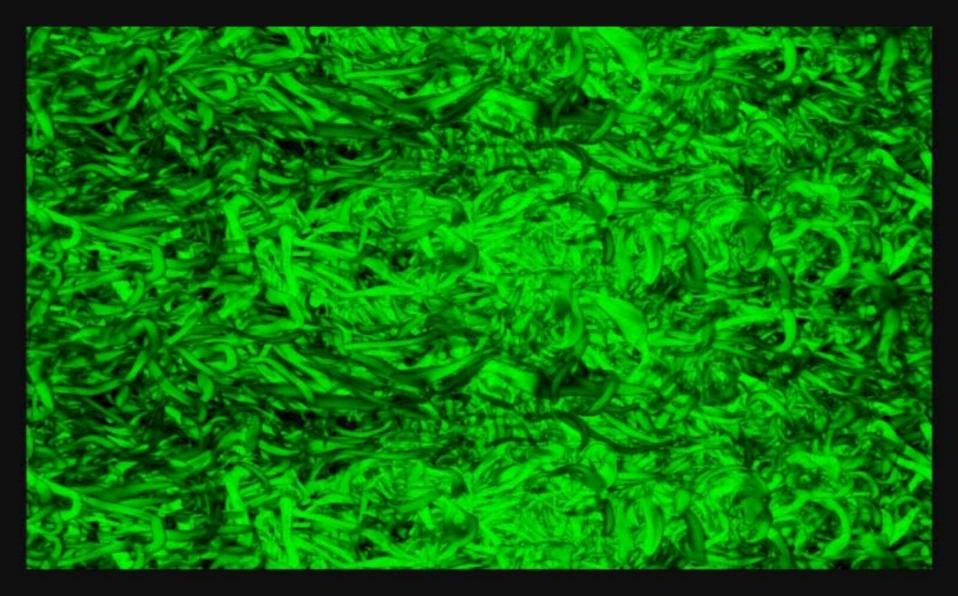




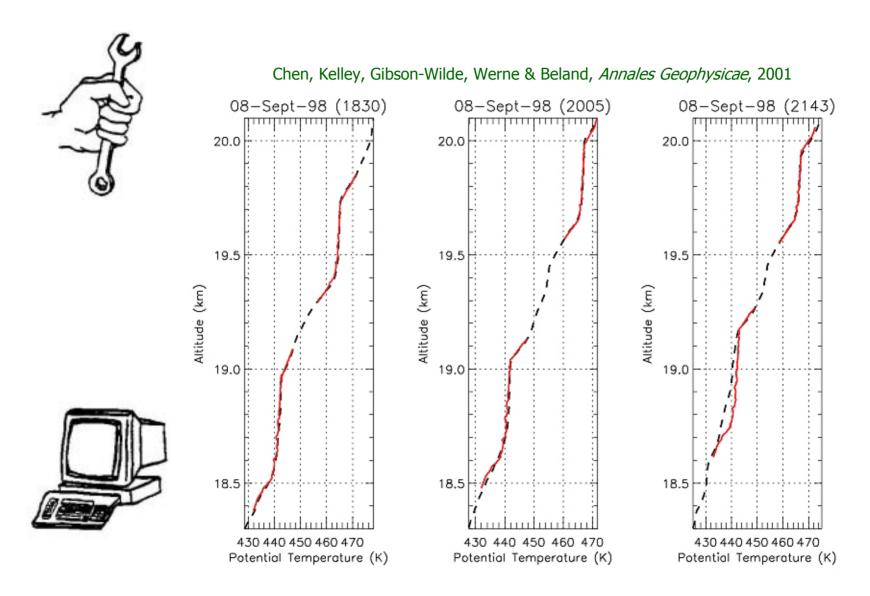


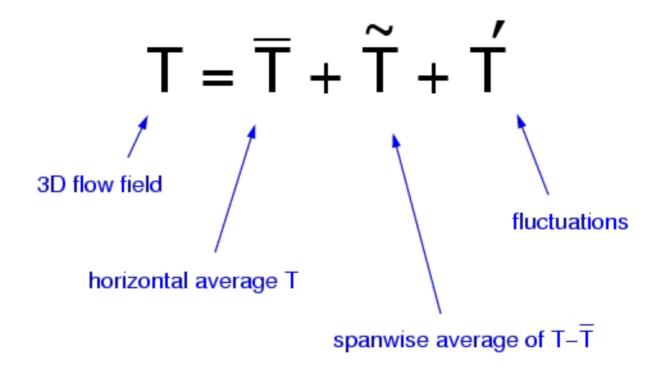




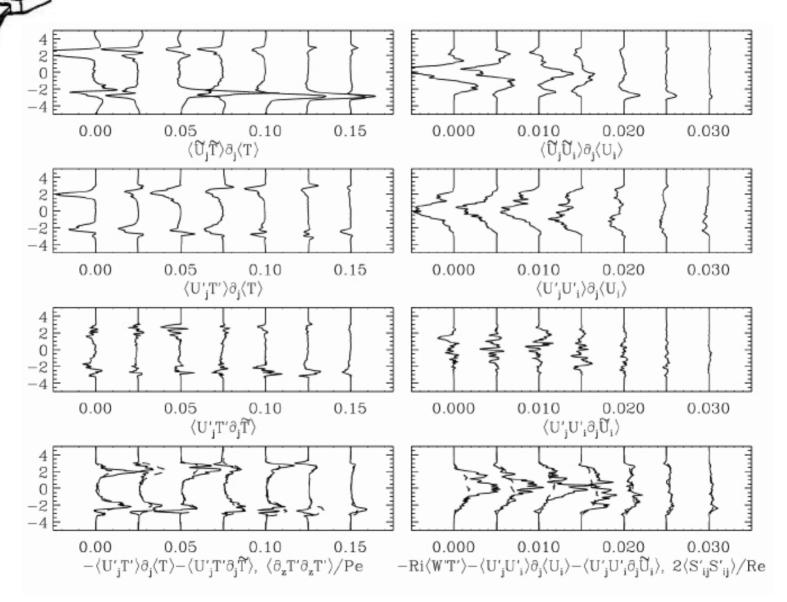


Wind shear: Balloon Comparison





Wind shear: production and dissipation



Stratified Turbulence Theory: thermal and viscous dissipation

Kolmogorov 1941

$$\Delta_{r}^{2}T = C_{\theta}^{-1/3} \epsilon \chi r$$

$$\Delta_r U = C \epsilon r$$

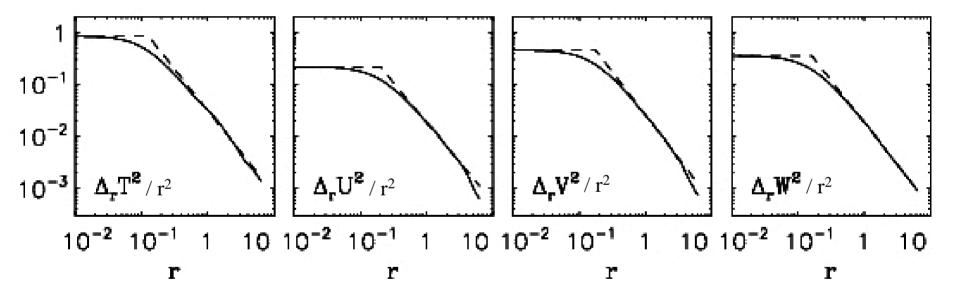
Bolgiano 1959

$$\Delta_{r}^{2} T = C_{\theta}^{-2/5} Ri \chi r$$

$$_{r}^{2}$$
 $_{r}^{4/5}$ $_{r}^{2/5}$ $_{r}^{6/5}$

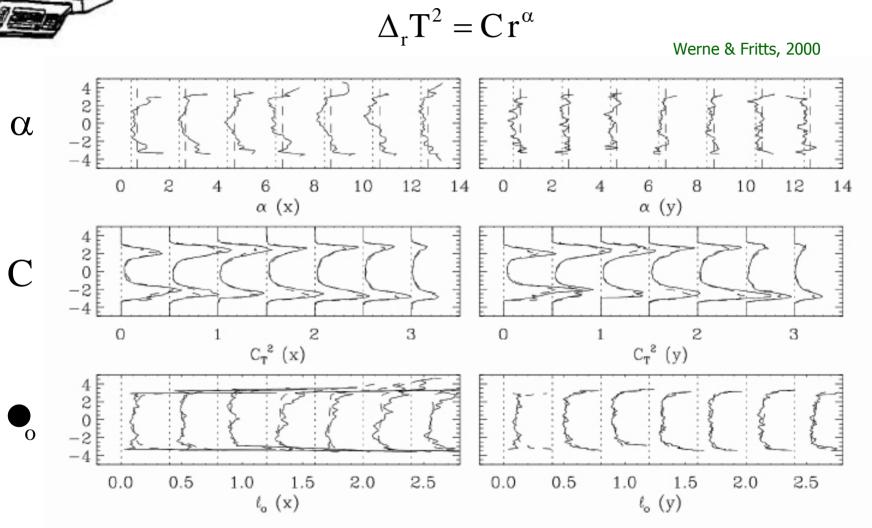


Wind shear: 2nd-order structure-function fits



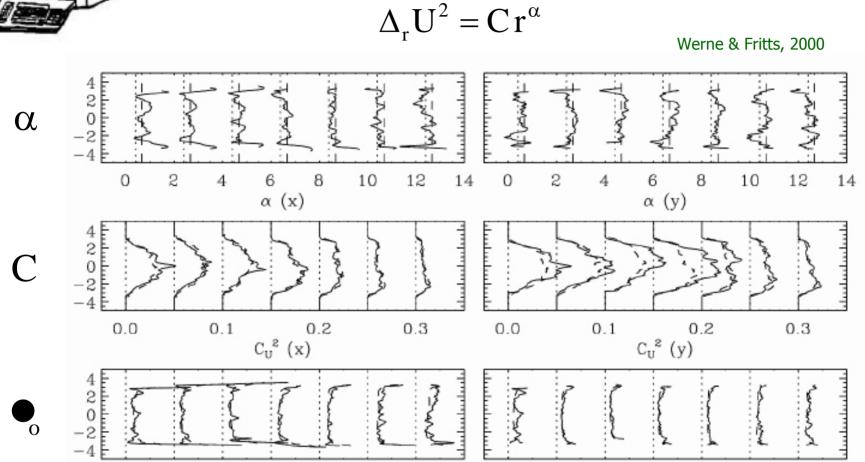


Wind shear: 2nd-order structure-function fits





Wind shear: 2nd-order structure-function fits



0

2

 $\ell_o(x)$

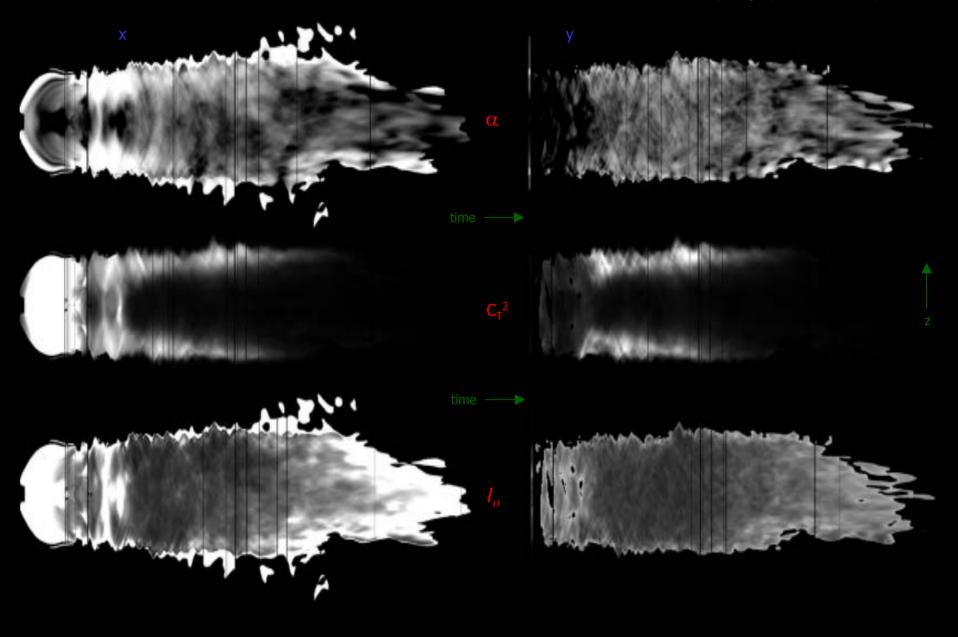
0

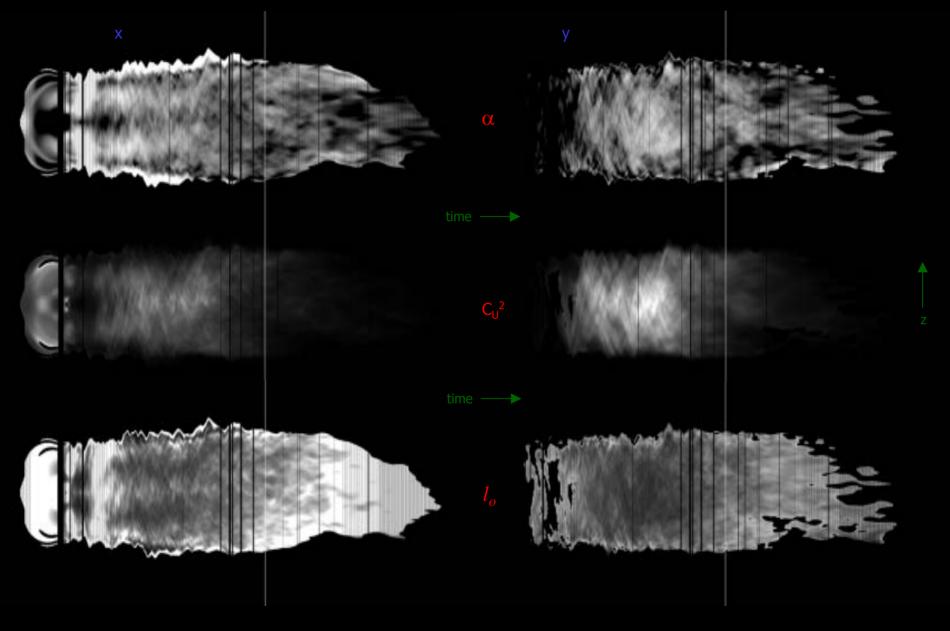
2

l_o (y)

6

6

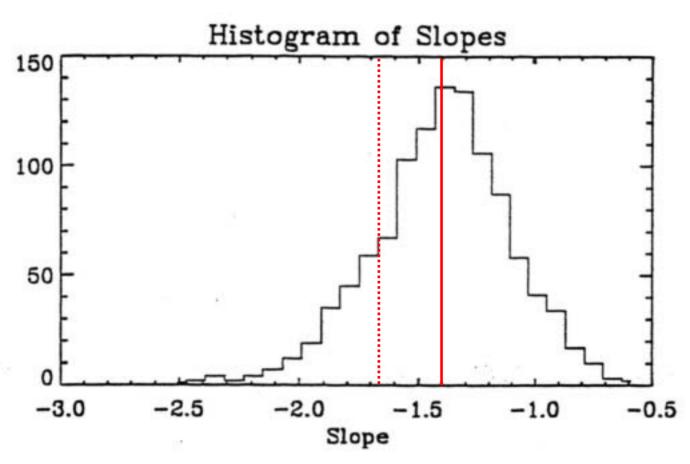






ABLE ACE anemometry data

Bruce Masson, 1996

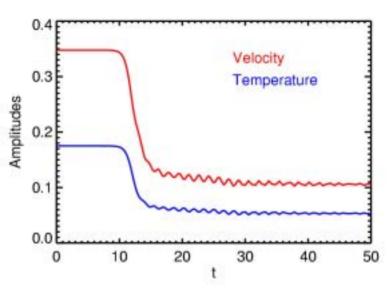


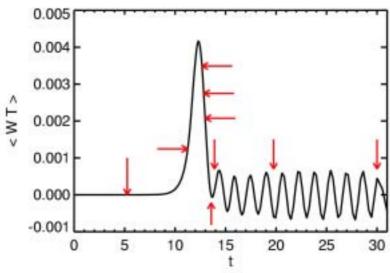
also, Michael Roggeman, private communication, 2001



Gravity Wave: Evolution

Bizon, Werne & Fritts, 2001





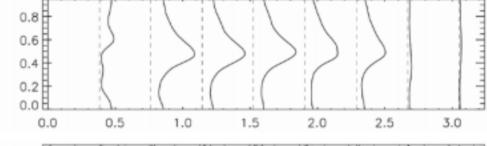
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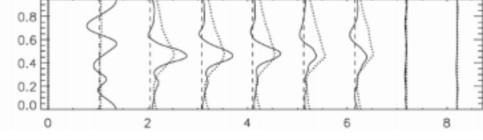
Gravity wave: Production and Dissipation



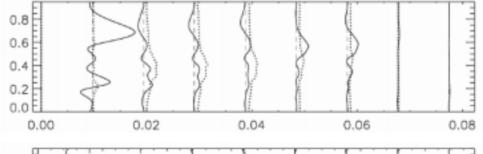
KE



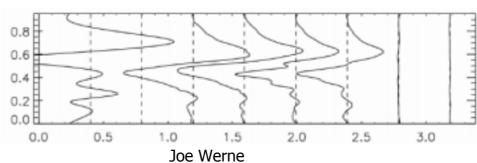
KE prod., €



PE prod., χ



 $d < pv_n > /dn$



- 1. Stratification restricts mixing dynamics to vertically confined regions.
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- 3. Mixing in the interior of turbulent layers reduces thermal gradients.

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- 4. Mixing zones in wind-shear simulations duplicate morphology exhibited by cloud observations.
- 5. Potential-temperature profiles, duration, C_T^2 profiles, and Ri profiles agree with balloon measurements.
- 6. Turbulence constants C_{θ} and C (relating χ and E to C_T^2 and C_U^2) obtained from comparison with the middle of a simulated shear layer agree with atmospheric measurements, as do the spectral slope and inner scale.

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- 7. Breaking gravity waves, in the absence of shear, dissipate rapidly.
- 8. Gravity-wave breaking is inherently out of balance.
- 9. Entrainment zones are non-stationary, inhomogeneous, and anisotropic; unfortunately they also have the greatest impact on optical propagation.

DNS Efforts

- Validate simulations
- ☐ Characterize/quantify atmospheric turbulence

Phase Screen Specification

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- Quantify non-Kolmogorov effects

Turbulence Simulation Algorithm Development

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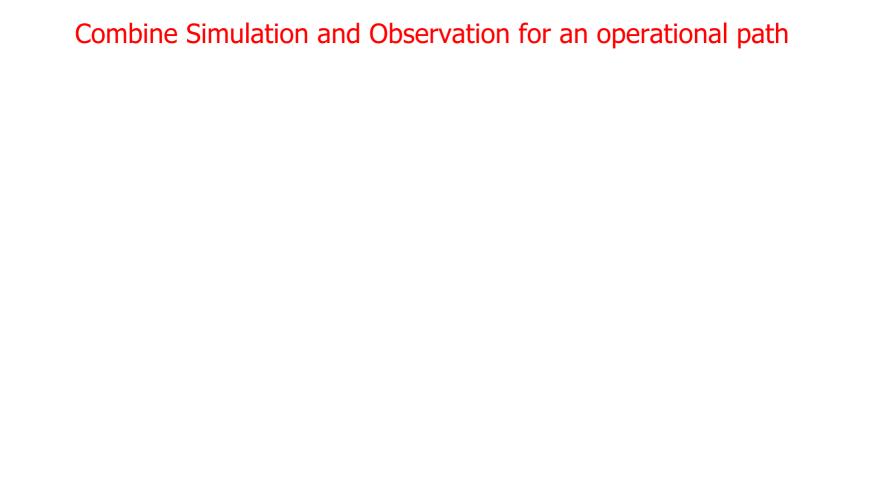
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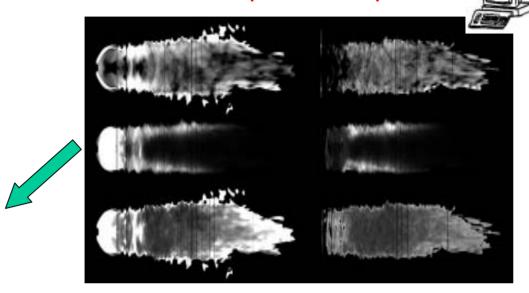
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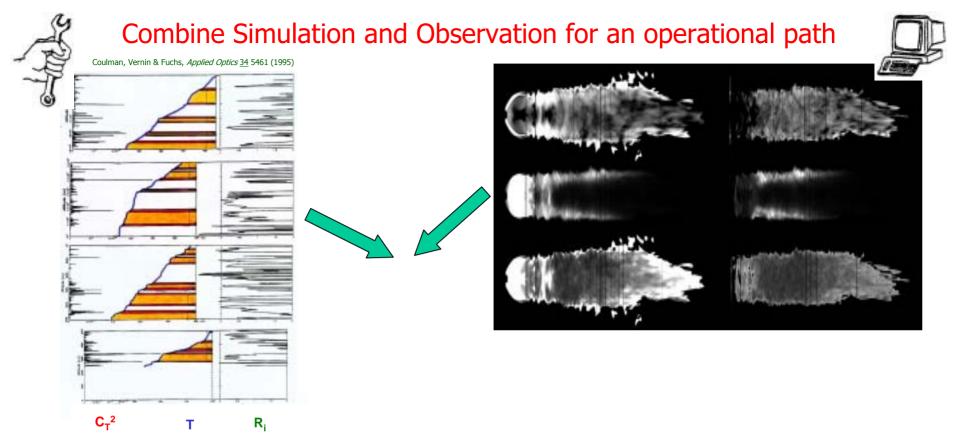
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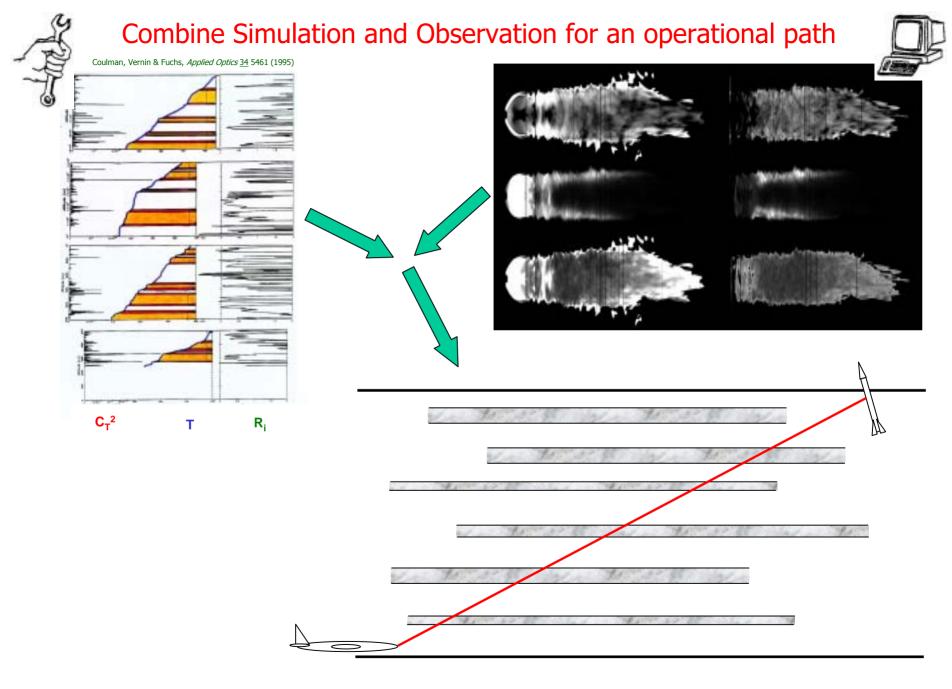
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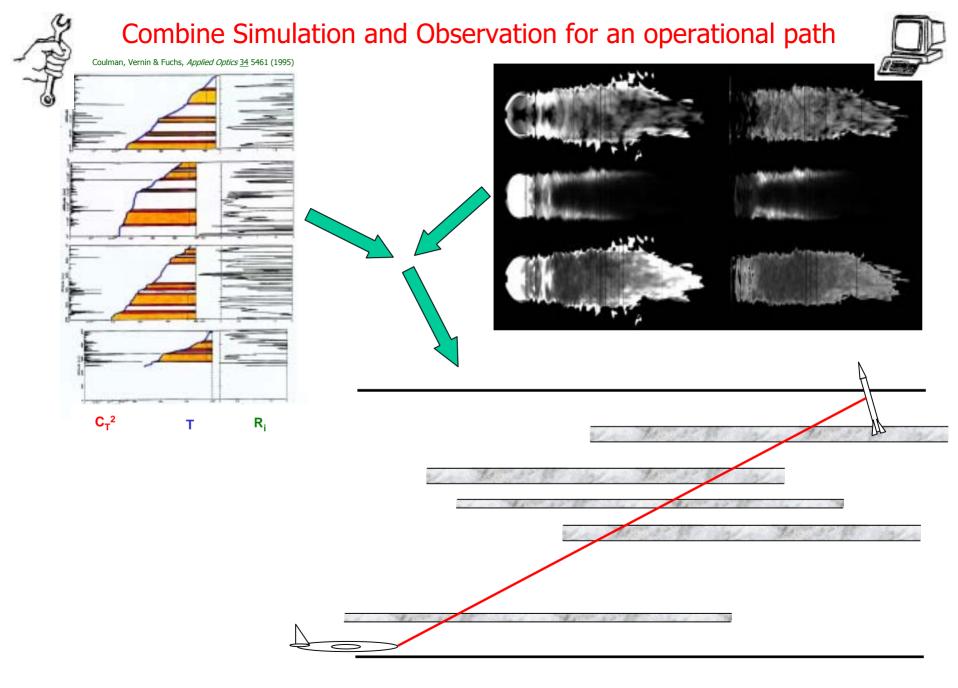


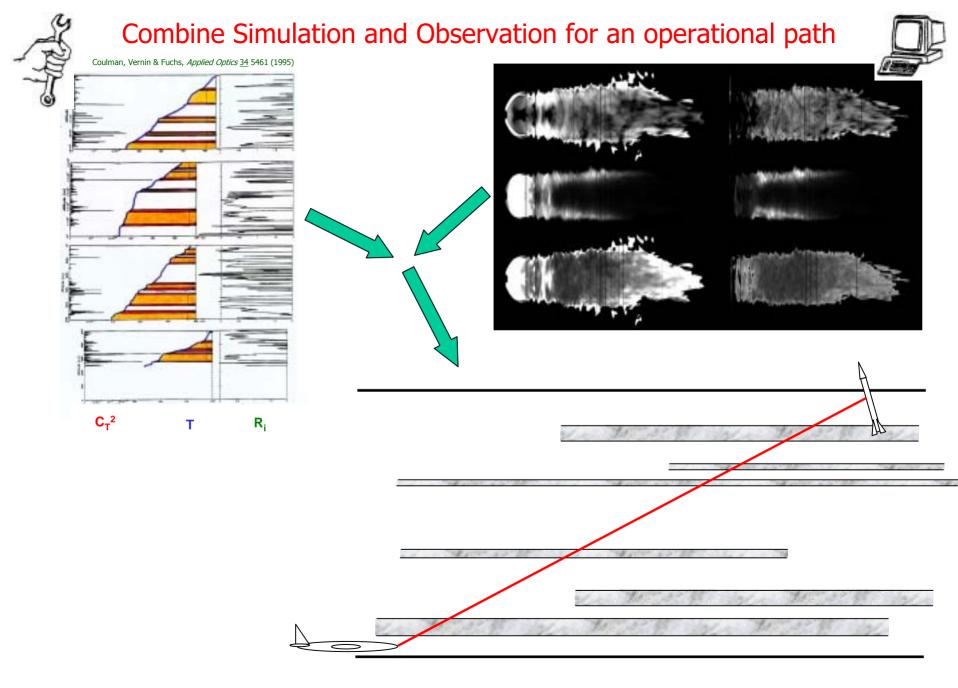
Combine Simulation and Observation for an operational path

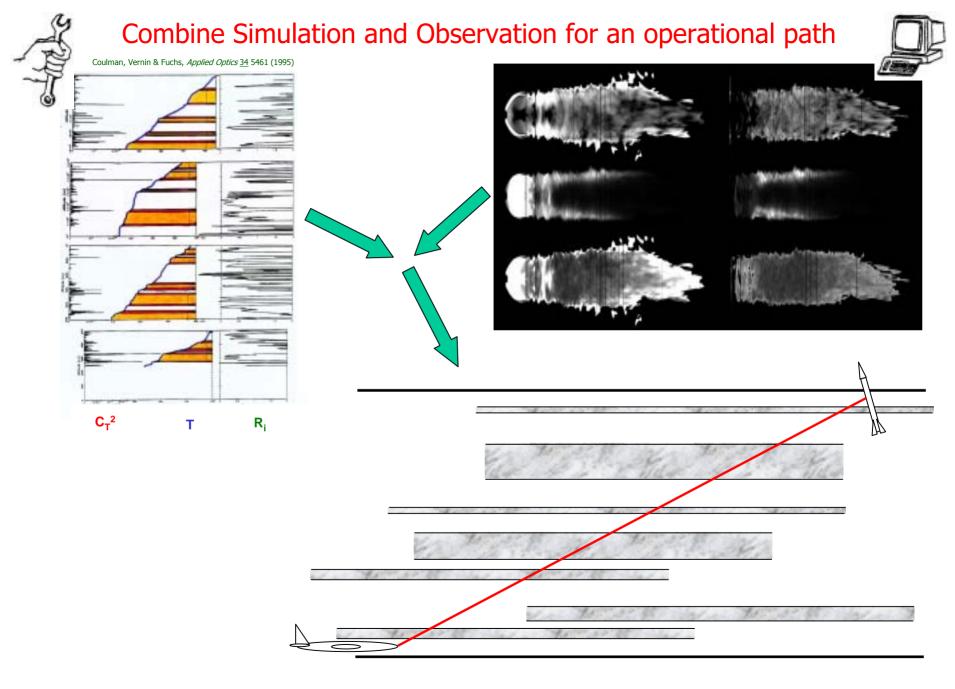


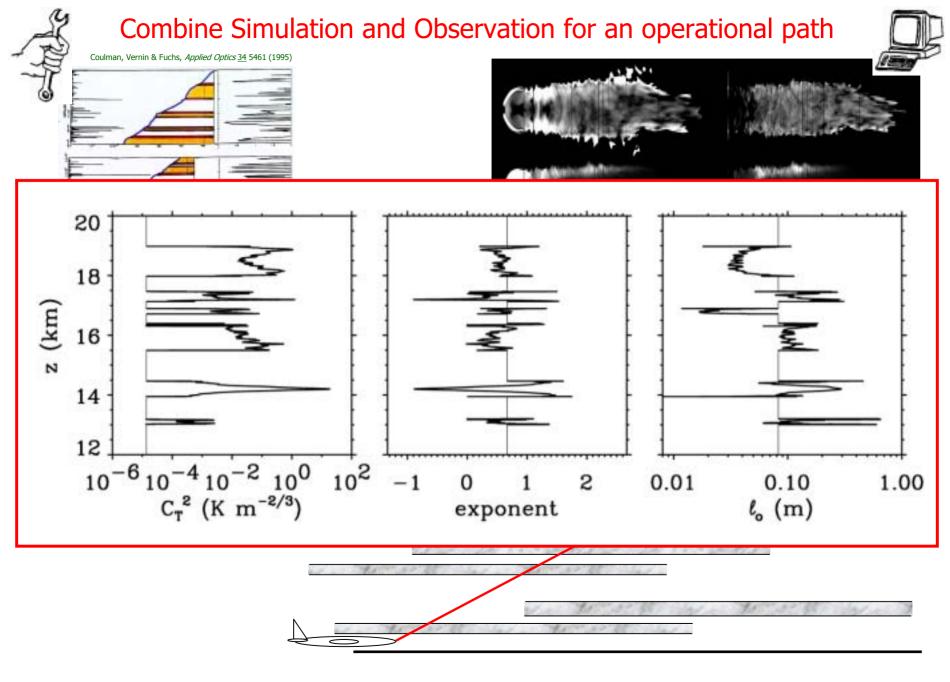












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RESOLVED FIELDS AND SFS MOMENTUM FLUXES

$$U_i = \overline{U_i} + u_i \equiv \int U_i(x'_j)G(x_i, x'_j)dx'_j + u_i$$

The SFS fluxes in LES are:

$${\cal T}_{ij} = \overline{U_i U_j} - \overline{U_i} \ \overline{U_j}$$

RESOLVED FIELDS AND SFS MOMENTUM FLUXES

$$U_i = \overline{U_i} + u_i \equiv \int U_i(x_j')G(x_i, x_j')dx_j' + u_i$$

The SFS fluxes in LES are (Germano, 1986):

$$\mathcal{T}_{ij} = \overline{U_i U_j} - \overline{U_i} \ \overline{U_j} = L_{ij} + C_{ij} + R_{ij}$$

$$\begin{array}{ll} \text{``Leonard''} & L_{ij} &= \overline{\overline{U_i} \ \overline{U_j}} - \overline{\overline{U_i}} \ \overline{\overline{U_j}} \\ \text{Cross} & C_{ij} &= \overline{\overline{U_i} u_j} + \overline{\overline{U_j} u_i} - \overline{\overline{U_i}} \overline{u_j} - \overline{\overline{U_j}} \overline{u_i} \\ \text{Reynolds} & R_{ij} &= \overline{u_i u_j} - \overline{u_i} \ \overline{u_j} \end{array}$$

Galilean invariant

Modeling τ_{ij}

Modeling au_{ij}

- Eddy viscosity models $T_{ij} = -2\nu_t S_{ij}$
 - Smagorinsky $\nu_t = (C_s l)^2 |S|$
 - TKE $\nu_t = C_k l \sqrt{E_s}$
 - length scale $l=\Delta_f$ and l=f(S,N)

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- Mixed models $T_{ij} = L_{ij} 2\nu_t S_{ij}$
 - L_{ij} depends on the resolved field

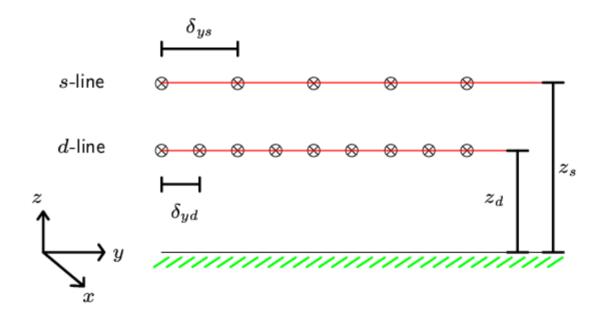
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Horizontal Array Turbulence Study (HATS) was designed to test SGS techniques.

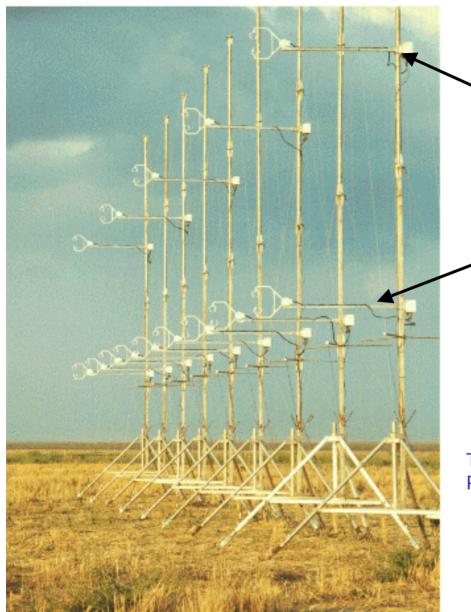
HORIZONTAL ARRAY TURBULENCE STUDY (HATS)

- Field campaign to measure T_{ij} , $T_{i\theta}$ over a wide range of stratification Horst et~al.~(2002) NCAR, JHU, PSU
- ullet Based on the horizontal array technique Tong et al. (1998), (1999) and Porté-Agel et al. (2001)
- 38 cases, 4 different sonic arrays, -2 < z/L < 2



HATS data is available from T. Horst, horst@ucar.edu

Horizontal Array Turbulence Study (HATS)



Four different sonic arrays, 38 cases

$$z = 6.90m$$
, $dy = 6.70m$

$$z = 8.66m$$
, $dy = 4.33m$

$$z = 8.66m$$
, $dy = 2.17m$

$$z = 5.15m$$
, $dy = 0.63m$

$$z = 3.45m$$
, $dy = 3.35m$

$$z = 4.33m$$
, $dy = 2.17m$

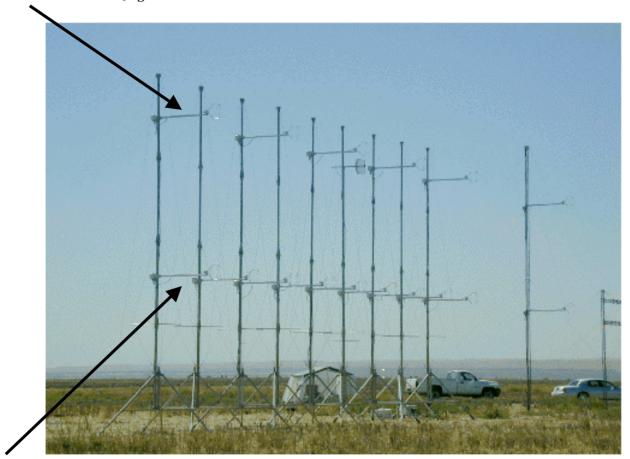
$$z = 4.33m$$
, $dy = 1.08m$

$$z = 4.15m$$
, $dy = 0.50m$

Tom Horst et al (2002), NCAR, JHU, PSU Pete Sullivan, NCAR

ARRAY-2

$$z_s = 8.66m, dy_s = 4.33m$$



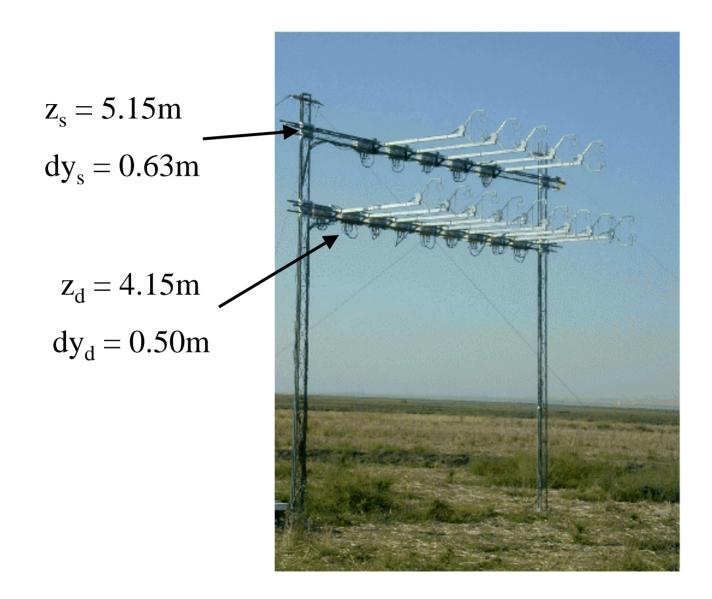
 $z_d = 4.33m$, $dy_d = 2.17m$

$$z_d = 8.66m$$
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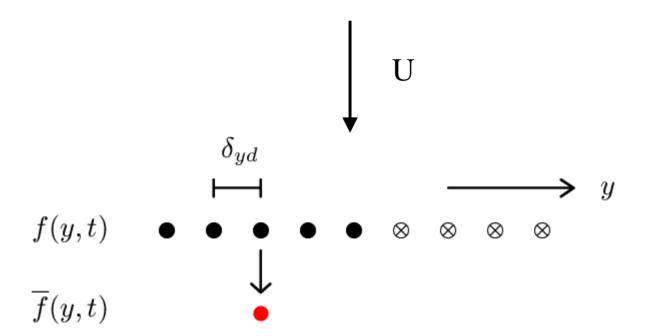


$$z_s = 4.33$$
m, $dy_s = 1.08$ m

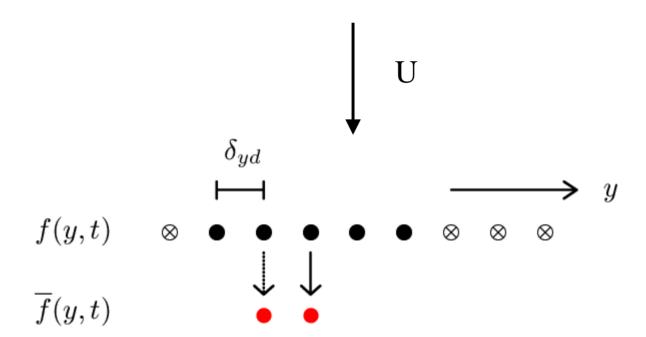
ARRAY-4



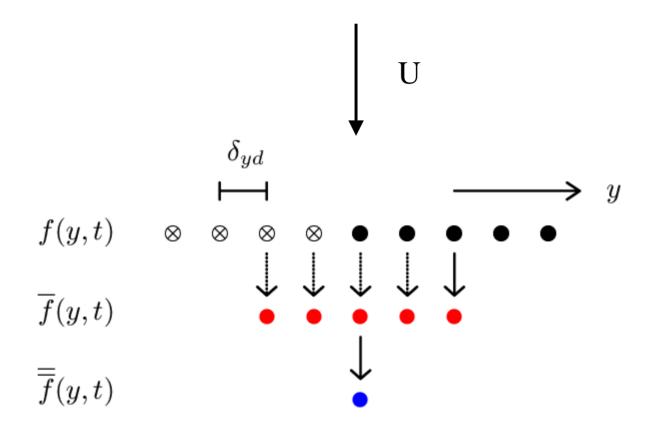
AN EXAMPLE OF LATERAL (Y) FILTERING



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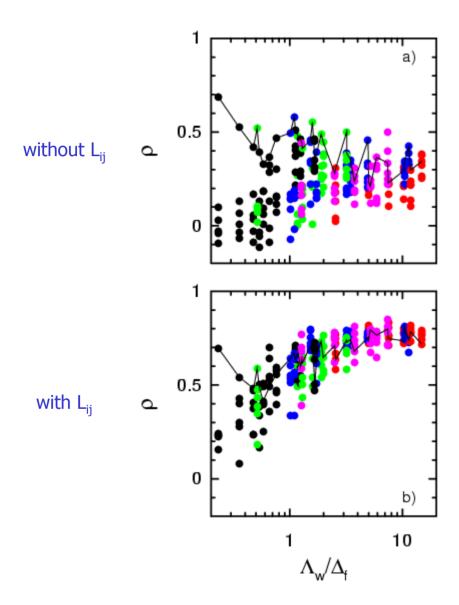


AN EXAMPLE OF LATERAL (Y) FILTERING



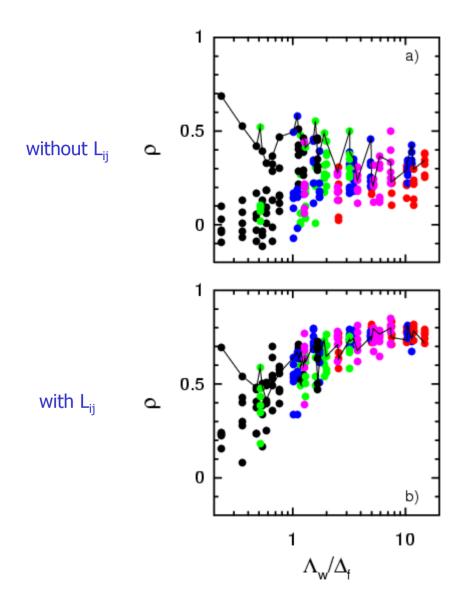
We use top-hat filtering in \boldsymbol{y} and Gaussian filtering in \boldsymbol{x} or t

Model-Data Correlations



Model-Data Correlations

Practical Computation of Lii



$$L_{ij} = \overline{\overline{U_i} \ \overline{U_j}} - \overline{\overline{U_i}} \ \overline{\overline{U_j}}$$

$$\overline{\overline{U_i}\ \overline{U_j}} \approx \overline{U_i}\ \overline{U_j} + \frac{\Delta_f^2}{24} \frac{\partial^2 \overline{U_i}}{\partial x_k \partial x_k} + H.O.T.$$

$$\overline{\overline{U_i}} \approx \overline{U_i} + \frac{\Delta_f^2}{24} \frac{\partial^2 \overline{U_i}}{\partial x_k \partial x_k} + H.O.T.$$

$$L_{ij} \approx \frac{\Delta_f^2}{12} \frac{\partial \overline{U_i}}{\partial x_k} \frac{\partial \overline{U_j}}{\partial x_k}$$



Linear Boussinesq Equations

$$\partial_t u + \partial_x p = 0$$
$$\partial_t w + \partial_z p - Ri \theta = 0$$
$$\partial_t \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

Linear Boussinesq Equations

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Plane Waves

$$\begin{pmatrix} u \\ w \\ \theta \end{pmatrix} = \begin{pmatrix} -k_x k_z \\ k_x^2 \\ k_x^2 / i\omega \\ -\omega k \end{pmatrix} e^{i(\mathbf{k} \cdot \mathbf{x} - \omega t)}$$

Linear Boussinesq Equations

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 Dispersion Relation
$$\omega^2/Ri = k_x^2/k^2$$

$$k_x^2 + k_z^2 = k^2$$

$$\omega^2/Ri = k_x^2/k^2$$

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Dispersion Relation

$$\omega^2/Ri\,=k_x^2/k^2$$

$$k_x^2 + k_z^2 = k^2$$

Elliptic Equation for Pressure (How should we handle BC's?)

$$\nabla^2 p = Ri \partial_z \theta$$

Linear Boussinesq Equations

$$\partial_t u + \partial_x p = 0$$

$$\partial_t w + \partial_z p - Ri \theta = 0 \quad (1)$$

$$\partial_t \theta + w = 0 \quad (2)$$

$$\nabla \cdot \mathbf{u} = 0$$

Plane Waves

$$\partial_{t}u + \partial_{x}p = 0$$

$$\partial_{t}w + \partial_{z}p - Ri\theta = 0 \quad (1)$$

$$\partial_{t}\theta + w = 0 \quad (2)$$

$$\nabla \cdot \mathbf{u} = 0$$
Dispersion Relation
$$\omega^{2}/Ri = k_{x}^{2}/k^{2} \quad (3)$$

$$k_{x}^{2} + k_{z}^{2} = k^{2}$$

Dispersion Relation

$$\omega^2/Ri = k_x^2/k^2$$
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$$k_x^2 + k_z^2 = k^2$$

Elliptic Equation for Pressure (How should we handle BC's?)

$$\nabla^2 p = Ri \, \partial_z \theta$$



Klemp & Durran (1983): Solve (1) & (2) subject to (3)

$$\left(Ri - \omega^2\right)w = -\omega k_z P$$

Linear Boussinesq Equations

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$$\partial_t w + \partial_z p - Ri \theta = 0 \quad (1)$$

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Dispersion Relation

$$\omega^2/Ri = k_x^2/k^2 \tag{3}$$

Elliptic Equation for Pressure (How should we handle BC's?)

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For low frequency ...

$$P \approx w\sqrt{Ri}/k_x$$

Linear Boussinesq Equations

Unlear Boussinesq Equations
$$\partial_t u + \partial_x p = 0$$

$$\partial_t w + \partial_z p - Ri \theta = 0 \quad (1)$$

$$\partial_t \theta + w = 0 \quad (2)$$

$$\nabla \mathbf{u} = 0$$

$$\partial_t w + \partial_z p - Ri \theta = 0 \quad (2)$$

$$\partial_t \theta + w =$$

Plane Waves

$$\begin{pmatrix} u \\ w \\ \theta \\ p \end{pmatrix} = \begin{pmatrix} -k_x k_z \\ k_x^2 \\ k_x^2 / i\omega \\ -\omega k_z \end{pmatrix} e^{i(\mathbf{k} \cdot \mathbf{x} - \omega t)}$$

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$\frac{\partial_t u + \partial_x p = 0}{\partial_t w + \partial_z p - Ri \theta = 0 \quad (1)}$ $\frac{\partial_t \theta + w = 0 \quad (2)}{\nabla \mathbf{u} = 0}$ \mathbf{u} $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (1)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (1)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} p - Ri \theta = 0 \quad (2)$ $\frac{\partial}{\partial t} w + \frac{\partial}{\partial t} \frac{$

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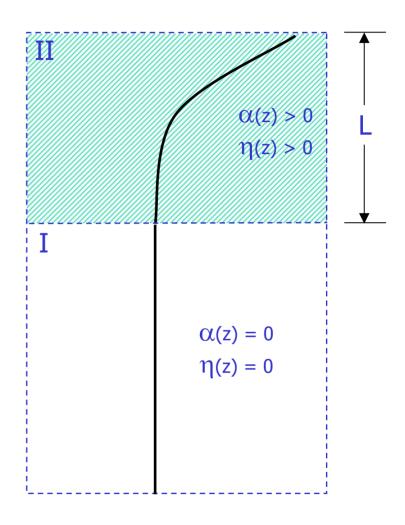
OK if kz>>kx, but other waves are trapped!

For low frequency ...

$$P \approx w\sqrt{Ri}/k_x$$





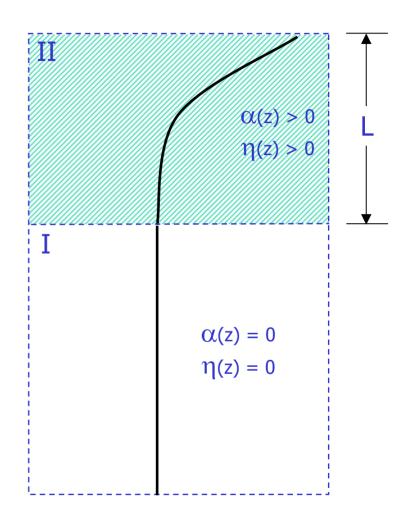




Linear Boussinesq Equations

$$[\partial_t + \underline{\alpha(z)}] u + \partial_x p = 0$$
$$[\partial_t + \underline{\alpha(z)}] w + \partial_z p - Ri \theta = 0$$
$$[\partial_t + \underline{\eta(z)}] \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

$$\nabla^2 p = Ri \,\partial_z \theta - \underline{\alpha(z)}' w$$





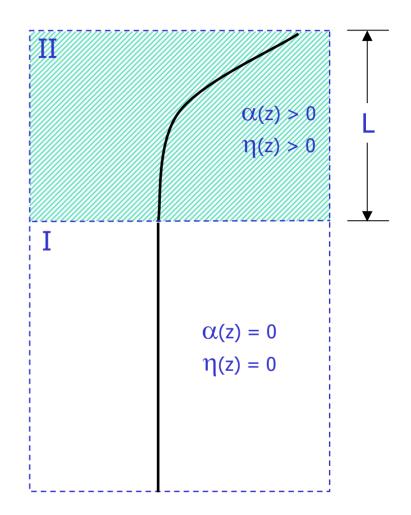
Linear Boussinesq Equations

$$[\partial_t + \alpha(z)] u + \partial_x p = 0$$
$$[\partial_t + \alpha(z)] w + \partial_z p - Ri \theta = 0$$
$$[\partial_t + \eta(z)] \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

1. If $\alpha(z)$ too small, reflections from outer boundary.

 $\nabla^2 p = Ri \, \partial_z \theta - \alpha(z)' w$

- 2. If $\alpha(z)$ too large, reflections from inner boundary.
- 3. If $\lambda > L$, reflect from II \rightarrow must make L large.

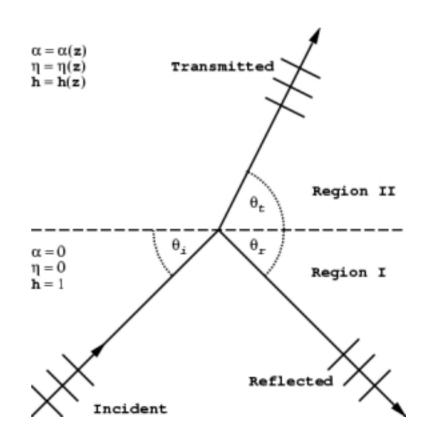




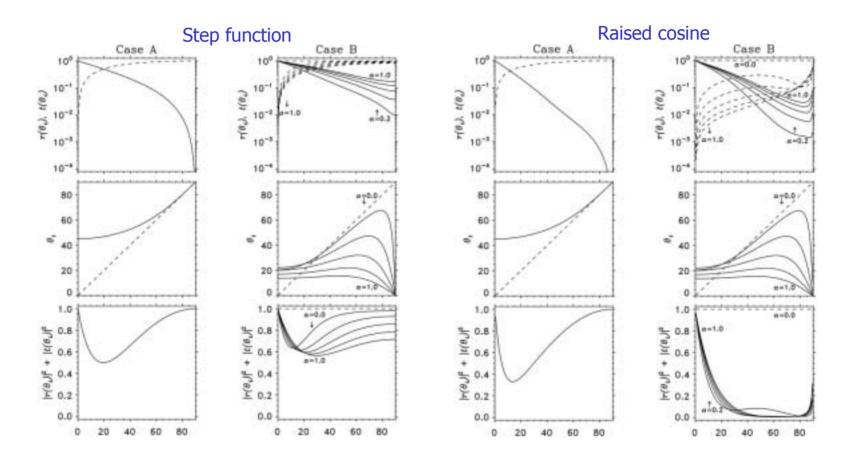


Linear Boussinesq Equations

$$[\partial_t + \alpha(z)] u + \partial_x p = 0$$
$$[\underline{h(z)}\partial_t + \alpha(z)] w + \partial_z p - Ri \theta = 0$$
$$[\partial_t + \underline{\eta(z)}] \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$







1. Reflection is reduced at high θ .

2. Smooth variation decreases reflection.







Try a different approach: Start with the solution you want.



Try a different approach: Start with the solution you want.

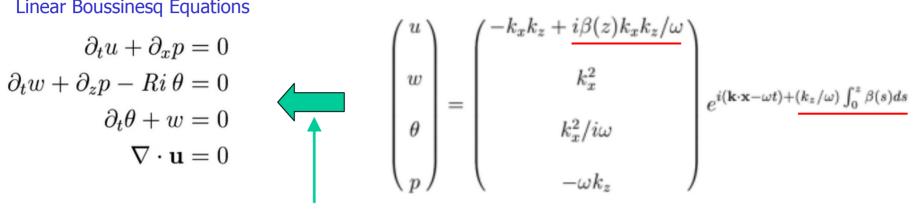
Damped Plane Waves

$$\begin{pmatrix} u \\ w \\ \theta \\ p \end{pmatrix} = \begin{pmatrix} -k_x k_z + i\beta(z)k_x k_z/\omega \\ k_x^2 \\ k_x^2/i\omega \\ -\omega k_z \end{pmatrix} e^{i(\mathbf{k}\cdot\mathbf{x} - \omega t) + (k_z/\omega)\int_0^z \beta(s)ds}$$



Try a different approach: Start with the solution you want.

Linear Boussinesq Equations



Damped Plane Waves

Dispersion Relation

$$\omega^2/Ri = k_x^2/k^2$$



Try a different approach: Start with the solution you want.

Linear Boussinesg Equations

$$\partial_t u + \partial_x p = 0$$
$$\partial_t w + \partial_z p - Ri \theta = 0$$
$$\partial_t \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$



Damped Plane Waves



$$\omega^2/Ri = k_x^2/k^2$$

$$\begin{aligned} \partial_t u + \partial_x p &= -U_0 \beta \\ \partial_t w + \partial_z p - Ri \, \theta &= -W_0 \beta \end{aligned} \qquad \text{where} \qquad U_0 &= \hat{p} k_x / \omega \\ \partial_t \theta + w &= 0 \qquad \qquad W_0 &= -\hat{p} k_z / \omega \\ \nabla \cdot \mathbf{u} &= 0 \end{aligned}$$

where
$$U_0 = \hat{p}k_x/\omega$$
 $W_0 = -\hat{p}k_z/\omega$



Try a different approach: Start with the solution you want.

Linear Boussinesg Equations

$$\partial_t u + \partial_x p = 0$$

$$\partial_t w + \partial_z p - Ri \theta = 0$$

$$\partial_t \theta + w = 0$$

$$\nabla \cdot \mathbf{u} = 0$$

Damped Plane Waves



$$\omega^2/Ri \, = k_x^2/k^2$$

$$\partial_t u + \partial_x p = -U_0 \beta$$
$$\partial_t w + \partial_z p - Ri \theta = -W_0 \beta$$
$$\partial_t \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

where
$$U_0 = \hat{p}k_x/\omega$$
 $\partial_t U_0 = -\partial_x \hat{p}$ $\partial_t U_0 = -\partial_x \hat{p}$ $\partial_t U_0 = \partial_z \hat{p}$

$$\partial_t U_0 = -\partial_x p$$
$$(\partial_t - \beta) W_0 = \partial_z \hat{p}$$



Try a different approach: Start with the solution you want.

Linear Boussinesg Equations

$$\partial_t u + \partial_x p = 0$$
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$$\partial_t \theta + w = 0$$
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Damped Plane Waves

$$\begin{pmatrix} u \\ w \\ \theta \\ p \end{pmatrix} = \begin{pmatrix} -k_x k_z + \underline{i\beta(z) k_x k_z/\omega} \\ k_x^2 \\ k_x^2/i\omega \\ -\omega k_z \end{pmatrix} e^{i(\mathbf{k}\cdot\mathbf{x} - \omega t) + (\underline{k_z/\omega}) \int_0^z \beta(s) ds}$$



Dispersion Relation

$$\omega^2/Ri\,=k_x^2/k^2$$

New System of Equations for Damping Layer (PML)

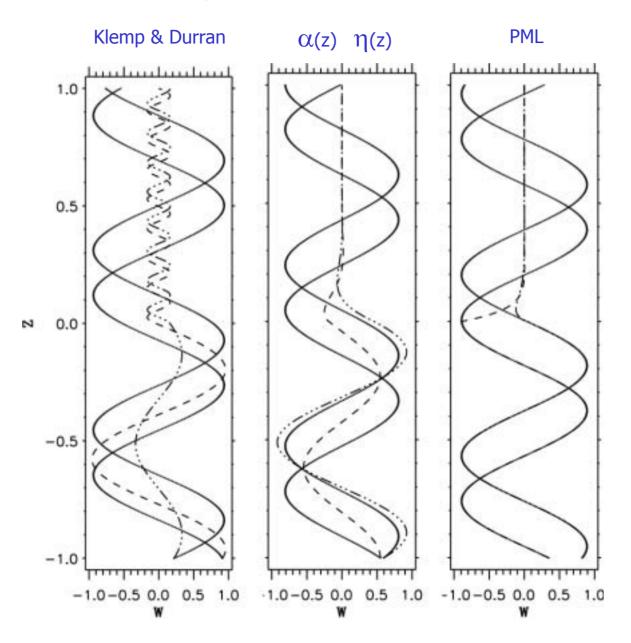
$$\partial_t u + \partial_x p = -U_0 \beta$$
$$\partial_t w + \partial_z p - Ri \theta = -W_0 \beta$$
$$\partial_t \theta + w = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

where
$$U_0 = \hat{p}k_x/\omega$$

$$W_0 = -\hat{p}k_z/\omega$$



$$\partial_t U_0 = -\partial_x \hat{p}$$
$$(\partial_t - \beta) W_0 = \partial_z \hat{p}$$



DoD UGC, June 20 CoRA, NWRA, Inc.



PML at finite Re

$$\left(\partial_{t} - Re^{-1}\nabla^{2}\right)u + \partial_{x}p = -U_{0}\beta - Re^{-1}\partial_{z}\left(2\partial_{z}U_{6}\beta - U_{5}\beta^{2} + U_{6}\beta'\right)$$

$$\left(\partial_{t} - Re^{-1}\nabla^{2}\right)w + \partial_{z}p - Ri\theta = -W_{0}\beta + Re^{-1}\partial_{x}\left(2\partial_{z}U_{6}\beta - U_{5}\beta^{2} + U_{6}\beta'\right)$$

$$\left(\partial_{t} - Pe^{-1}\nabla^{2}\right)\theta + w = -Pe^{-1}\left(2\partial_{z}\theta_{3}\beta - \theta_{2}\beta^{2} + \theta_{3}\beta'\right)$$

$$\nabla \cdot \mathbf{u} = 0$$

$$\partial_t U_0 = -\partial_x p$$
$$(\partial_t - \beta) W_0 = \partial_z p$$

$$(\partial_t - \beta) U_6 = -u$$
$$(\partial_t - \beta) U_5 = -\partial_z U_6$$
$$(\partial_t - \beta) \theta_3 = -\partial_z \theta$$
$$(\partial_t - \beta) \theta_2 = -\partial_z \theta_3$$

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- 2. Abarbanel, Gottlieb & Hesthaven, 1999: Well-posed Perfectly Matched Layers for Advective Acoustics, *JCP* 154, 266-283.
- 3. Tam, Auriault & Cambuli, 1998: Perfectly Matched Layer as an Absorbing Boundary Condition for the Linearized Euler Equations in Open and Ducted Domains, *JCP* 144, 213-234.
- 4. Hesthaven, 1998: On the Analysis and Construction of Perfectly Matched Layers for the Linearized Euler Equations, *JCP* 142, 129-147.
- 5. Collino & Monk, 1998: The Perfectly Matched Layer in Curvilinear Coordinates, *Siam J. Sci. Comput.* **19**, 2061-2090.
- 6. Hu, 1996: On Absorbing Boundary Conditions for Linearized Euler Equations by a Perfectly Matched Layer, *JCP* 129, 201-219.

ABL Future Work Wish List

- Continued comparison with data
 - → CASES-99
 - → VTMX
 - → Air Force Balloon and Radar
- A priori tests and SGS development
 - Eddy-viscosity models
 - → Velocity-estimation models
 - Event catalog for meso-scale models
- Characterize nature of stratified turbulence
 - → Turbulence/billow/mean-flow
 - → Stability profile
 - → Turbulence anisotropy
- Investigate impact of initial conditions
 - Amplitude and shape of noise spectrum
 - Optimal perturbations
 - Vary Ri and nonlinear thermal structure
- ☐ High-resolution wave-breaking solutions
- → High-Re incompressible solutions
- Spatial modulation and distribution of turbulence
 - Multiple billow/wave interactions
 - → Phase-screen specification using combined DNS/observation results

ABL-Related Publications

- Chen, Kelley, Gibson-Wilde, Werne & Beland, 2001: "Comparison of observed lower atmospheric turbulent structures with a direct numerical simulation" *Annales Geophysicae*, (in press).
- Dubrulle, Laval, Sullivan & Werne, 2001: "A new dynamical subgrid model for the planetary surface layer. I. The model and a priori tests" *J. Atmos. Sci.* (in press).
- Werne, Bizon, Meyer & Fritts, 2001: "Wave-breaking and shear turbulence simulations in support of the Airborne Laser" 11th DoD UGC, Biloxi.
- Werne & Fritts, 2001: "Anisotropy in a stratified shear layer" *Physics and Chemistry of the Earth*, **26**, 263.
- Werne, Adams & Sanders, 2001: "Hierarchical Data Structure and Massively Parallel I/O" *Parallel Computing* (submitted).
- Werne & Fritts, 2000: "Structure Functions in Stratified Shear Turbulence" 10th DoD HPC UGC, Albuquerque.
- Fritts & Werne, 2000: "Turbulence Dynamics and Mixing due to Gravity Waves in the Lower and Middle Atmosphere" in Atmospheric Science across the Stratopause, Geophysical Monograph 123, American Geophys. Union, 143-159.
- Gibson-Wilde, Wene, Fritts & Hill, 2000: "Direct numerical simulation of VHF radar measurements of turbulence in the mesosphere" *Radio Sci.* 35, 783.
- Hill, Gibson-Wilde, Werne & Fritts, 1999: "Turbulence-induced fluctuations in ionization and application to PMSE" *Earth Planets Space*, **51**, 499.
- Werne & Fritts, 1999: "Stratified shear turbulence: Evolution and statistics" *Geophys. Res. Lett.*, 26, 439.
- Werne & Fritts, 1999: "Anisotropy in Stratified Shear Turbulence" 9th DoD HPC UGC, Monterey.
- Werne & Fritts, 1998: "Turbulence in Stratified and Sheared Fluids: T3E Simulations" 8th DoD HPC UGC, Houston.